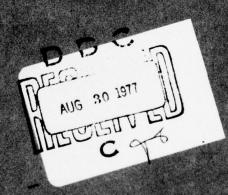


NSWE/DL TR-3868 PRELIMINARY EASTERN INDIAN OCEAN GEOID FROM GEOS-3 DATA



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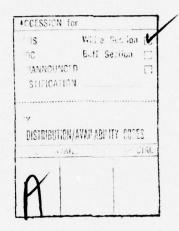
SAMUEL L. SMITH, IN ALAN C. CHAPPELL

Warfare Analysis Department

JONE 1977



NSWC/DL TR-3668 June 1977



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APPROVED FOR PUBLIC RELEASE; DISTRIBUTION UNLIMITED

FORWORD

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INTRODUCTION

The use of satellite radar altimeter measurements to derive an ocean geoid that contains geoid undulation information at much shorter wavelengths than can be obtained from classical analysis of satellite orbit perturbations has been postulated for a number of years, e.g. references 1 and 2. Some experiments in this direction were carried out with radar altimeter data from Skylab, e.g. references 3 and 4, but the amount of Skylab radar altimeter data and the lack of accuracy of the Skylab orbital ephemerides precluded geoid determination over any appreciable area.

The GEOS-3 satellite was launched on 9 April 1975, carrying a radar altimeter with both short pulse and long pulse capability, laser retroreflectors and a Doppler beacon to allow precise orbit determination. GEOS-3 has produced radar altimeter data of both good quality and quantity for over a year. Both theoretical studies, reference 5 and preliminary evaluations, reference 6, of the GEOS-3 data showed that the short pulse radar altimeter data had a lower noise level than the long pulse data and would result in more precise derived geoids.

This paper develops the preliminary derivation of a local geoid in the Eastern Indian Ocean from 94 passes of short pulse GEOS-3 radar altimeter data received by the DoD telemetry station at Perth, Australia. This data was taken over a 34 day period in July-August 1975. The orbital ephemerides used in the analysis were obtained from Doppler tracking data and have an estimated accuracy of 2 meters in the radial component, reference 7.

This preliminary derivation of the geoid does not consider tide effects on the altimeter measurements which could introduce uncertainties of about 0.5 meters. Also, the standard tropospheric range correction used on the data could result in errors in individual measurements of up to 25 centimeters. A technique for reducing all the biases by analyzing the radar altimeter measurements at track intersections is employed. A later analysis is planned that will include data from other telemetry stations in the area whose coverage overlaps the Perth coverage and extends the total time span of the data set to several months. It will include tidal corrections to the data before the bias removal and geoid derivation is carried out.

The preliminary GEOS-3 geoid derived in the paper is compared with the Marsh and Chang 1976 Geoid, ref. 8. Correlations of larger features in the GEOS-3 geoid with bottom topography are also given.

PROCEDURE

Averaging at Intersections

Ninety-four passes of short pulse radar altimetry data were taken by the Perth, Australia telemetry station and processed at NSWC/DL using precise short-arc Doppler derived satellite ephemerides. For each pass time, latitude, longitude, geoid height and along-track deflections of the vertical were computed at 0.1 second time intervals. Details of this processing, including the Wiener filter used, may be found in reference 9. Nine of the passes contained data too fragmented for efficient operation of the Wiener filter and were eliminated from the following analysis. The remaining 85 passes were used. The ground tracks of these passes are given in Figure 1. differences in geoid height at each of the 716 intersections of these passes are given in Table 1. The average difference of geoid height over all the intersections is 75 cm with a standard deviation with respect to the mean of 2.3 meters. The maximum difference is 7.83 meters. As a first approximation to the geoid, the average of the two geoid heights at each intersection is taken as the geoid height and contours of constant geoid height plotted. Since alongtrack deflection of the vertical is available for each track at each intersection, the surface gradient at each intersection may be computed. This is used as an interpolation aid in plotting the geoid height contours. A geoid derived in this manner is given in Figure 2. The +'s in Figure 2 represent the location of the intersections. The contour interval in Figure 2 is 2 m. The General Purpose Contouring Program by California Computer Products was used to generate the contours in Figure 2 and all subsequent contour plots.

Bias Removal

If one studies the intersections in Table 1, it is seen that some passes have all positive differences, e.g. descending pass 1580, or all negative differences. e.g. descending pass 1837. Since pass 1580 is intersected by 19 other passes taken over a time span of 33 days and pass 1837 is intersected by 16 other passes taken over a time span of 32 days, one could assume that different tidal phases, different deviations from the standard troposphere, different orbit uncertainties on the crossing passes would be sampled. Therefore the intersections would be expected to be more random unless the single pass, i.e. 1580 or 1837, was biased with respect to the other passes. Using this assumption each pass in Table 1 has been adjusted so that the sum of the intersection differences with the crossing passes have been minimized. The mean bias adjustment is 0 cm; thus the mean

geoid is not changed. The standard deviation of the biases is 2.2 m. The amount of the adjustment of each pass is given in Table 2. The intersection differences after applying the adjustments are presented in Table 3, where the average difference summed over all intersections is now 9 cm with a standard deivation of 83 cm with respect to the mean and a maximum difference of 3.15 m. The geoid heights are again taken as the midpoint at each intersection and a contour map is made as before using the surface gradient at each intersection to aid in interpolation.

RESULTS

Comparison With the Marsh and Chang 1976 Geoid

The preliminary eastern Indian Ocean geoid derived from the GEOS-3 measurements using the bias removal technique described above is given in Figure 3. The +'s plotted on Figure 3 indicate the locations of the intersections. Figure 4 is a plot of the Marsh and Chang 1976 Geoid. A contour plot of the differences between the GEOS-3 Geoid after bias removal and the Marsh and Chang 1976 Geoid is given in Figure 5. The contour interval in Figures 3,4, and 5 is 2 m. In general the agreement is good, with major features such as the through running from the southwestern tip of Australia toward the northwest, and the saddle point south of Australia comparing well. The maximum difference between the two geoids is 7 m. To further compare the two geoids, the along-track geoid heights (after bias removal) from pass 1419 and descending pass 1724 are compared in Figures 6 and 7, with the Marsh and Chang 1976 geoid heights along these tracks. Again the agreement is quite good, with the GEOS-3 along-track data showing more fine structure than was apparent in the overall geoid plots, since the GEOS-3 contour plots used information only at the intersections instead of at every point along-track. Both the GEOS-3 Geoids and the Marsh and Chang 1976 Geoid were referenced to an ellipsoid with a semi-major axis of 6378.135 km and a flattening reciprocal of 298.26.

Comparison with Bottom Topography

Comparison of the GEOS-3 Geoid was made with larger bottom topography features of the eastern Indian Ocean. Figure 8 is a contour map of a small area of the geoid with a one meter interval between contour lines. Figure 9 is a three dimensional projection of the same area shown in Figure 8. Comparison of Figures 3, 8 and 9 with ocean bottom charts shows good agreement with large features. An attempt was made to correlate the GEOS-3 Geoid with finer scale bottom topographic features

shown on a detailed charts supplied by the Naval Oceanographic Office without much success, probably due to the smoothing of the GEOS-3 Geoid by using data only at intersections in its construction. Much success was had by making along-track comparisons where the short wavelength information is not lost. Figure 10 shows an along-track comparison of bottom topography and geoid heights for pass 1746. Geoid heights are plotted for the GEOS-3 Geoid after bias removal as well as the along-track satellite data. The lack of short wavelength information in the GEOS-3 Geoid is evident. Correlation of the three curves is very good. The sea mount near the middle of the pass shows up clearly in the two geoid height curves. The sea mount is located approximately at lattitude -22°2 and longitude 104°6. The geoid undulations caused by this sea mount can be seen in figures 2,3,4,8, and

CONCLUSIONS

Careful processing of GEOS-3 radar altimetry data with good orbit ephemerides can result in a derived ocean geoid that is accurate to about one meter. It is expected that greater accuracy will be obtained in the GEOS-3 Geoid with the analysis of additional data in the area from other telemetry stations whose coverage partially overlaps Perth and which will provide data over a longer time frame. Also the inclusion of tide and sea state corrections and a bias rate term in the analysis should result in greater accuracy in the derived geoid. The use of along-track data (instead of using only intersection data) should improve the accuracy and the short wavelength structure of the GEOS-3 Geoid.

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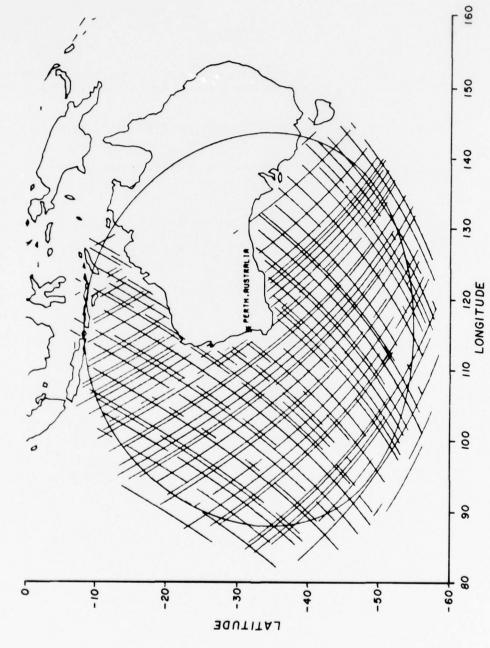


Figure 1

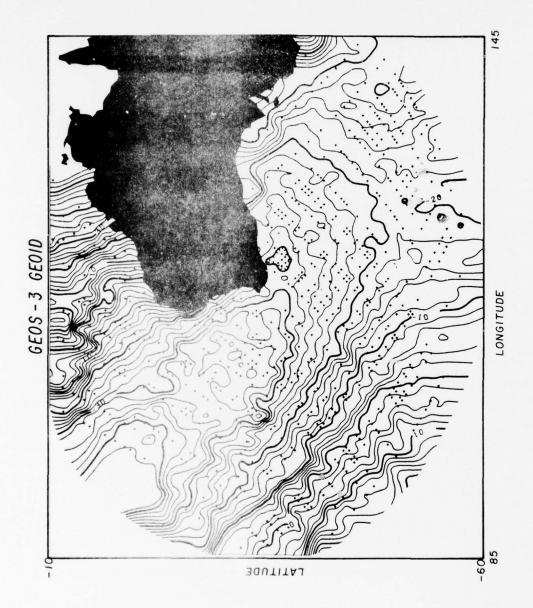


Figure 2

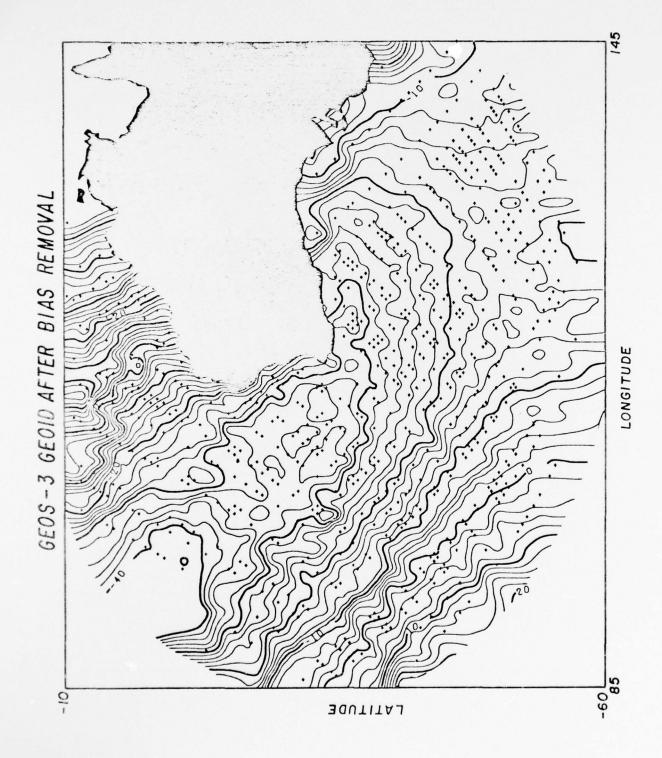


Figure 3

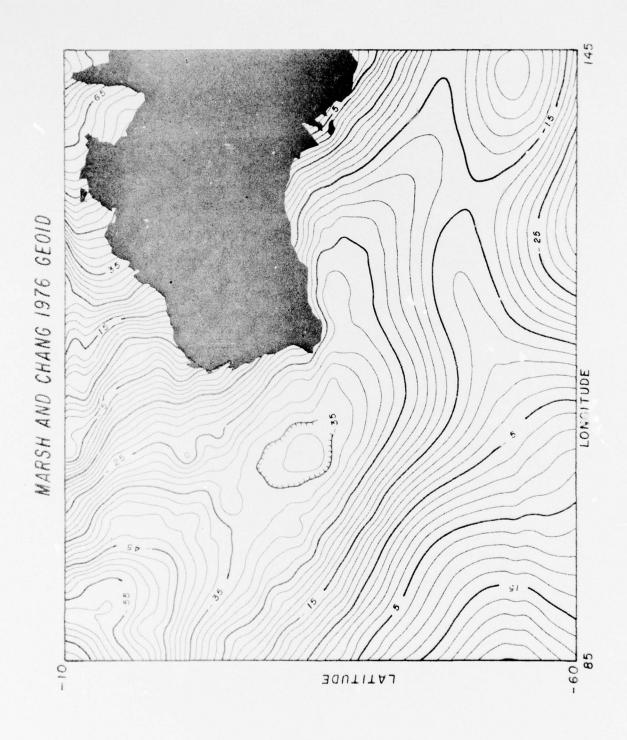


Figure 4

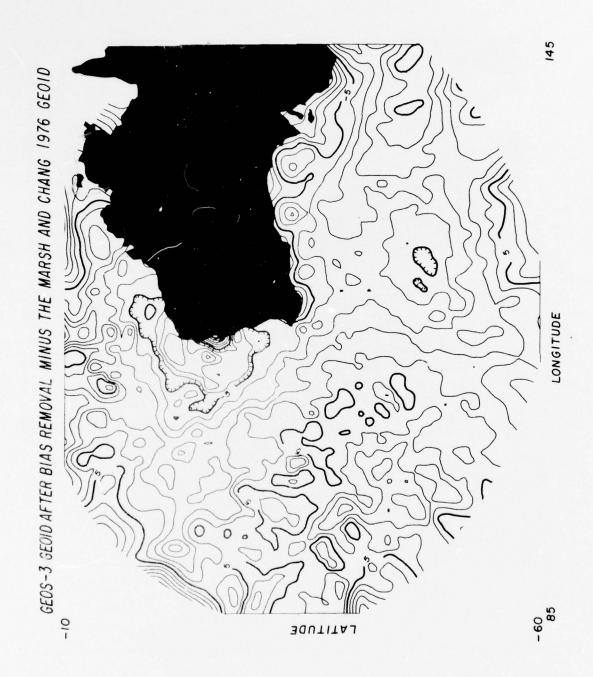
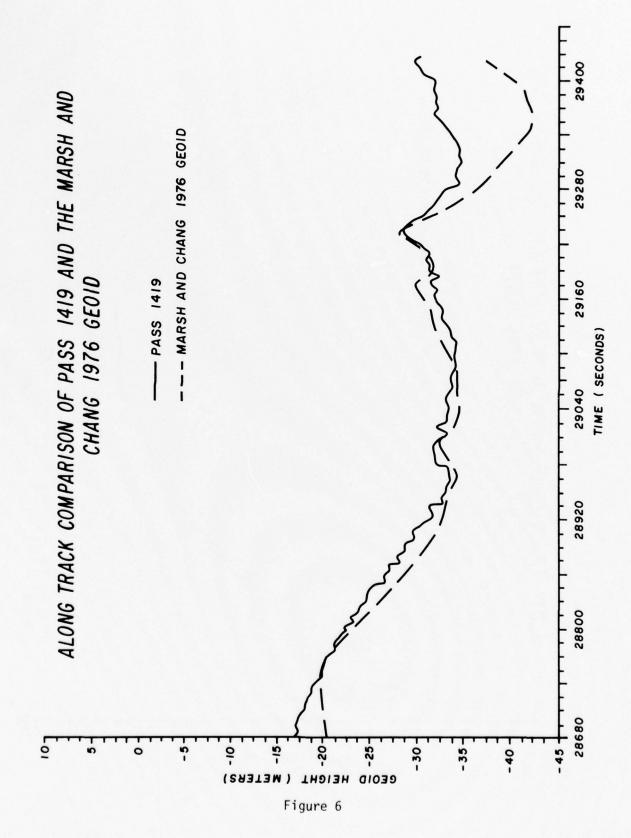
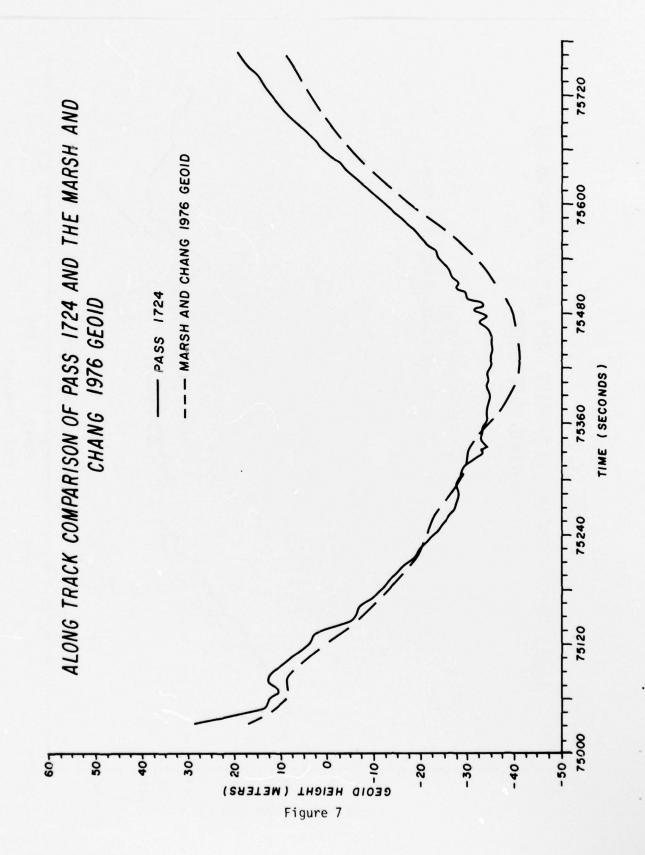


Figure 5





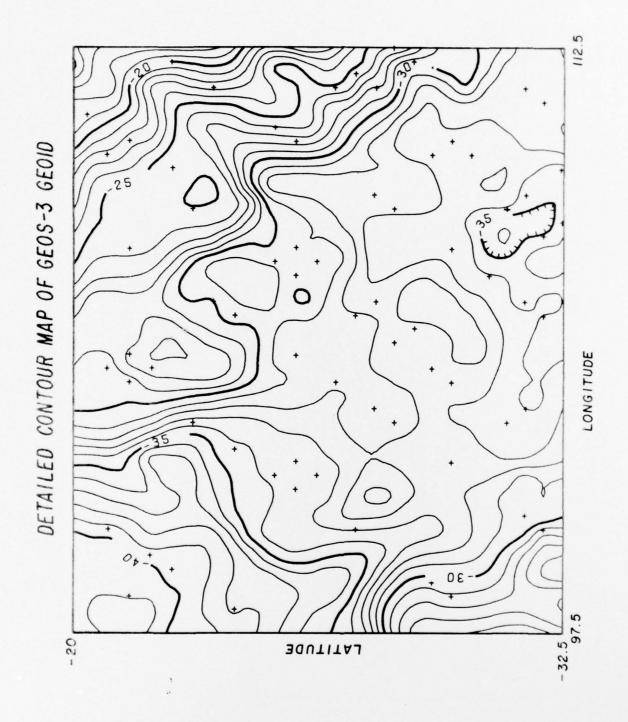


Figure 8

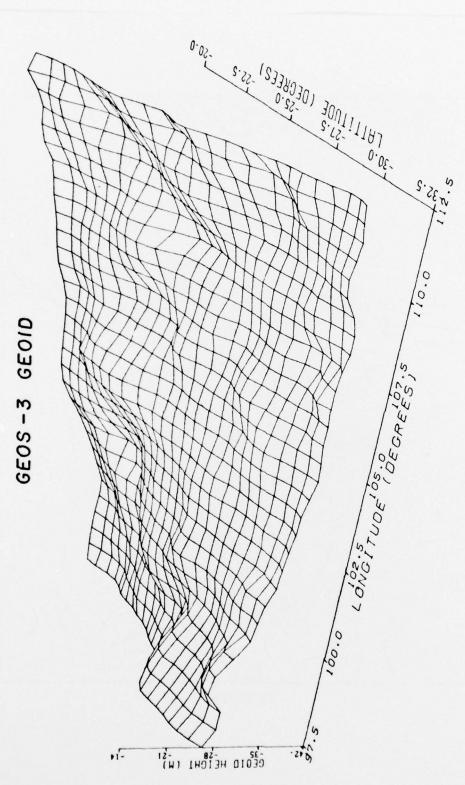


Figure 9

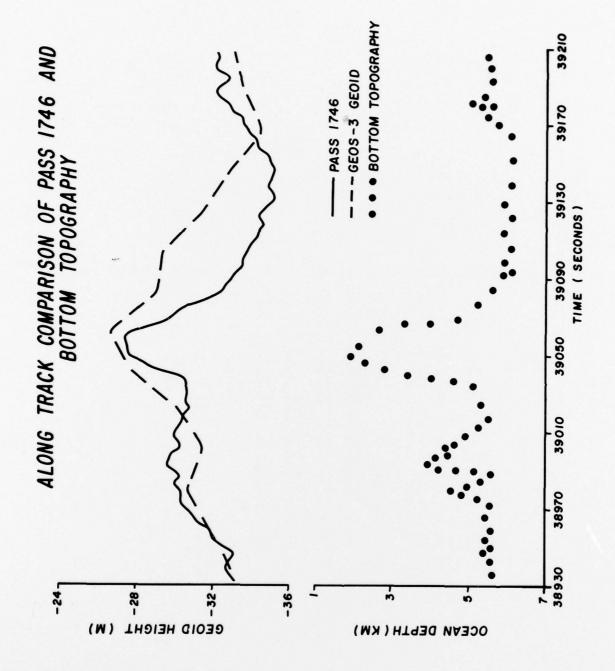


Figure 10

TABLE 1
GEOID HEIGHT DIFFERENCES AT INTERSECTIONS (METERS)

																			D	ESCE	DNIN	G PA	SSES			
cendin	g Passes	1354	1368	1382	1383	1396	1397	1410	1411	1424	1425	1426	1566	1568	1580	1581	1624	1637	1651	1652	1653	1665	1666	1667	1680	
		-2.14 -4.99 -1.18			-1.34	.70 33 -2.78 -1.82	42 -1.04	2.61 1.36 .57	3.22 1.84 .36 96 -2.21 61 3.90	2.26	10 -3.45	2.76		2.61 2.43 -1.43 -1.27	3.25 4.17 2.87 2.48	. 28 93 -2.48	1.02 -3.38 -2.41 1.93	4.99 3.50 3.35	2.18 3.70 2.49 2.19	71 .86 -3.18 -2.06	2.92 3.67 .86 -1.10 44 3.15	.66 1.92 .35	.60 -2.17	3.16 .62 -1.48	2.83 4.60 3.15 15 2.35 1.52	-1
sasse	1434 1447 1561 1575 1633 1646 1647		17		2.63	-2.00 .86 1.55 .62 .74 2.12 96		.28 3.01 2.49 2.87 4.15 .66	35 3.81 2.59 3.70	3.73	-2.45 .36 -1.05	15 3.16 3.72		2.94	4.72	-2.33 .87 .09	-1.83 1.71	2.59 5.32	4.19	-2.15 .63 .50	4.18	2.23 1.72 2.04 3.39 .50	2.17 1.59 1.73 1.65 3.48 25	24 3.52 3.08 2.58 1.65 2.80 1.14	4.73 4.49 4.56 5.62 2.49	3
d build	1660 1661 1662 1674					-1.49						.02		.14	2.40	-2.21 .21	-1.91 .87	3.17		-1.88 01	.41		68 .85	04	1.13	d
Ascer	1675	-2.30	-4.39	-2.95	1.95	-2.09 -1.13 1.57 25 -1.39 -2.32	-1.08 2.37 -1.41	52 1.04 2.92	-3.34 -1.05 2.35 .97 2.66 74		56	3.29	3.08	2.02 1.37 2.80	4.64 2.51	-1.08	-2.79 .37 -1.49	5.58	2.11 3.77 1.98	-2.49 .26 -1.25 .73 95	2.18 1.89 3.18 2.93 27	.17 2.63	.99 .43 2.65 .37	2.58 2.14 61	.58 2.45 4.50	1
								-1.04	-3.50			-1.33		-1.23	1.85		-2.80							-3.57	.07	
	1746		.11	-3.85	15 3.66		.62		4.35			.29 4.00		3.68	1.93	-2.37 .92	-2.14 2.19	2.10		-2.08 1.01	.89	62	2.00	.15 4.24		
	1775		-1.61 -3.24		2.03	.05 -1.18 .85	2.97 .46 2.97		2.55			72		2.77		53 -2.21 08	-2.96 .07 -1.59	2.77 4.76	1.91	51 -1.69 .36	.39	.54 2.14	43	1.98 .17 2.87	2.28 1.84 3.84	



TABLE 1

MEIGHT DIFFERENCES AT INTERSECTIONS (METERS)

D	ESCE	DNIN	G PA	SSES																			
51	1652	1653	1665	1666	1667	1680	1681	1682	1694	1696	1708	1709	1710	1722	1723	1724	1736	1737	1738	1739	1752	1809	1837
18 70 49	-3.18	2.92 3.67 .86 -1.10 44 3.15	.66 1.92 .35	2.35 .60 -2.17	2,33 1,85 3,16 ,62 -1,48 -1,99 -1,05	2.83 4.60 3.15 15 2.35 1.52	2.70 2.90 1.96 -1.49 83		4.14 3.02 .49 2.75 2.28	-3.07	2.84 3.78 2.13 2.53	-5.08	1.46 2.44 3.65 -2.11	1.52 2.23 1.29	74 .55 -3.47 -1.75	3.58 4.94 2.55 54 .14 3.19	1.06 2.74 1.86	2.82 1.15	2.00 2.68 1.99 .97 -1.21 -1.23 61			2.18 13 -1.53 -2.34 48	
19 62 32 75 89		3.15 .31 4.18 3.82 2.10 3.41 1.65 2.18	2.23 1.72 2.04 3.39 .50	69 2.17 1.59 1.73 1.65 3.48 25	- 24 3.52 3.08 2.58 1.65 2.80 1.14 1.94	1.66 4.73 4.49 4.56 5.62 2.49	-1.10 .08 3.30 3.12	1.15	1.94 5.03 4.34 4.41 6.07 2.16	94 1.98 2.79 2.13 1.95 29	4.61 4.23 4.77 1.67	-4.15 73 -1.03	.06 1.85 3.73 2.35 1.91 2.55 3.24 .77 2.26	3.46 2.58 2.77 4.60	-2.20 .98 .64 .53 .37	1.52 4.01 5.08 3.58 3.71 4.59 2.37 3.78	3.03 2.46 2.07 3.55	3.57 2.25 2.89 3.98 .49	.15 3.19 2.87 2.06 3.32 1.45		-3.89	2.86	-5.77 -1.74 -2.09
37	-1.88 01	.41		68 .85	-1.33 04 2.26		.27 .06		1.83	-1.60	2.24	-3.54 -1.29	74 1.24		-1.93 24	.59 1.31 2.57		.01	41 .36 2.06 -2.59			-1.74 .35	-5.03 -2.07
72 11 77 98 52	-2.49 .26 -1.25 .73 95	43 2.18 1.89 3.18 2.93 27 .99	.17 2.63	90 .99 .43 2.65 .37	-1.02 2.36 .54 2.58 2.14 61 .64 -3.57		-1.37 .84 1.21	3.01	2.04 4.83 2.40	-1.82 .72 .83 1.60 29	4.60	-4.63 -1.21 -3.08 -2.69 -3.72	-1,25 .81 1,49 3,16 1,97	.82 2.92	-3.02 .02 -1.45 1.01 -1.06	.32 2.96 2.59 4.31 3.21 1.38 1.81	3.21	72 2.10 1.51 3.44 .74	2.18 18 18 76 -2.87	2.59		1.10 1.52 .26	-6.55 -2.43
	-3.11	38	07	-1.56		.07	76.04		. 93	-2.21		-4.69	-1.50	.40	-2.70	.09	.67	60	57			-3.32	-5.99
	-2.08 1.01	.89	62	2.00	4.24		17 3.63		1.62	76 2.40		-4.16 74	2.56		-2.31 1.20	1.40 4.18	.62	2.92	3.75				-5.26 -1.25
91 44	-1.69 .36	.39 3.73	.54 2.14	09 43 1.93	1.98 .17 2.87	2.28 1.84 3.84	Z.05 .17		1.83 4.24	1.02	2.12 3.95	-1.97 -3.84	1.60 26 3.10		96 -1.37 .56	2.91 1.03 4.63	.81 2.48	.95 .47 2.48	2.25			1.92	

TABLE 2
BIASES (METERS)

Ascending Passes

Descending Passes

Pass No.	Bias	Pass No.	Bias
1347 1349 1362 1376 1390 1391 1404 1405 1406 1418 1419 1420 1433 1434 1447 1561 1575 1633 1646 1647 1660 1661 1662 1674 1675 1676 1689 1703 1704	2.0255 1.4120 .8006 2.6962 1.1268 -2.6197 .1451 -1.5824 2.7338 -2.8210 -1.1408 1.5730 2.9797 1.5557 2.3771 2.0308 3.6217 .1213 1.9914068984896609 .3416 -3.9360 -1.5822 .76760942 2.9032 1.0856	1354 1368 1382 1383 1396 1397 1410 1411 1424 1425 1426 1566 1568 1580 1581 1624 1637 1651 1652 1653 1665 1666 1667 1680 1681 1682 1694 1696 1708	Bias 2.0087 2.8957 3.64367709 .7984871991725216 -2.4272 1.57487826 -2.7478 -1.2155 -2.8077 1.4333 1.1353 -3.2068 -2.2751 1.2811 -1.3553746429337286 -2.34922807 -2.2569 -2.5601 .0629 -2.4820 3.1803
1717 1718 1731	6313 1651 -4.4150	1709 1710 1722	3.1803 9380 -1.3373 1.0554
1732 1745 1746 1747 1759 1775 1803	-1.6223 2.5125 8584 2.3044 -3.2807 .7127 5055 2.3792	1723 1724 1736 1737 1738 1739 1752 1809	-2.2592 -1.6476 -1.1118 5532 -2.2550 4.2271 .5532 4.4850

	3	

																G	EOID HEI	GHT DIFFE	RENCES	AT INTER	SECTIONS	AFTER B	IAS REMOVA
Descending Passes_13	54	1368	1382	1383	1396	1397	1410	1411	1424	1425	1426	1566	1568	1580	1581	1624	1637	1651	1652	1653	1665	1666	1667
1349 1362 1376 1390 1391 2.4 1404 -3.1 1405 1406 1418	19 13	.62	.70	21 15	-1.20 66 .64	68 -2.42 .70	-1.00 68 50 .74	1.29 .52 -1.29 1.14 -2.88 .45 .65	-1.30 27	.67	62		01 .41 03	36 -1.34 -1.06 47	.30	.75	91 83 01	89 -1.27 91 23	23 56 .72	.15 39 -1.63 .16 21	89 -1.52 -1.52 22	64 82 .16	.19 .32 27 -1.23 .41 -2.86 20 34
1419 1420 1433 1434 8 1447 8 1561 1575 8 1633	73	1.44	.49	55 .35	06 -1.32 .79 96 50 71 29	.59 60 -2.14 .36 -1.93	.50 89 .01 42 38 38	.27 .172 92 1.62	-1.08	.38	.20 .80 1.38		.15 51 .73	-1.07 -1.38 84 13	.24 .73 -1.45 .57 -1.02	.45 1.27 1.22	.52 87 82 -1.06 28	-1.06 -1.03 99 -1.15 50	.27 .33 .22	.10 16 .91 -1.63 -1.56	-1.49 -1.41 .74 98 36	.15 -1.10 26 94 67 43 67	.17 1.22 63 .29 -1.46
ut 1646 pu 1647 1660 1661 1.3 1662 16742	25	.15			03	-1.43	.23	.13			10		42	. 26	12 1.30	12 1.67	.63	-1.63	.06	-1.17	83 💂	31	78 -1.21 11 1.19
1675 1.2 1676 1.8 1689 1.7 1703 1704 1.8 1717 1718 1.6	73 39	.11	.79	.42	.29 24 54 54	37 -1.40 -1.65 .09	.14 .22 90	1.06 .54 1.05 63 1.14		1.11	65 .41 .58	75	52 .04 .25 .50	.06 -1.07 -1.38	30 .60 49 73	07 .74 26	.22 16 53 -1.10	.02 07 -1.41 -1.38 59	.38 .77 .12 89 75	20 .06 .63 -1.08 .49 -1.00 20	48 -1.01	.39 07 .24 55 -1.01 67	16 .86 09 -1.05 .33 71
1731 -1.4 1732 1.6 1745 1746 1747 1759		.12	. 65	94 06 .58	.10	.60	34	.39 .42 .74 1.52		.31	49 .37 .91		83	.67 -2.48 02 .07	32 07 .05	04 15 1.02	08 25		21 .06 01	11	.81 51	23 .12 60	.11 41 .28 1.20
1775 2.6 1803 1.5 1831		.57 .17		.54	.14 .12 73	1.38 .09 28	85 07 80	1.32			-1.00		.84 91 05	.12	.19 27 -1.03	1.46 .50 .05	.07	.14	.06 .10 73	46 00	.30	-1.10 22 74	.54 05 24

				ABLE 3																				
	T DIFFE 1651	RENCES A	T INTERS	SECTIONS 1665	AFTER B	IAS REMOV	1680	1681 .39	1682	1694	_1696	1708	1709	1710	1722	1723	1724	1736	1737	1738 -,57	1739	1752	1809	183
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Ninety-four passes of GEOS-3 short pulse radar July-August 1975 over the eastern Indian Ocean (by at Perth, Australia) have been analyzed to arrive the self consistency of the data at track intersec difference of 75 cm with a standard deviation of 2 cessing. Application of bias removal techniques redifference to 9 cm and improves the self consistence	the DoD telemetry station at a preliminary ocean geoid. tions has a mean geoid height .3 meters with normal proeduced the mean geoid height									

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standard deviation of less than 1 m. A comparison of the GEOS-3 Geoid is made with the NASA Marsh and Chang 1976 Geoid. The GEOS-3 Geoid correlates well with the larger features of the local bottom topography.